

A weakest-link analysis for fatigue strength of components containing defects

POLITECNICO DI MILANO



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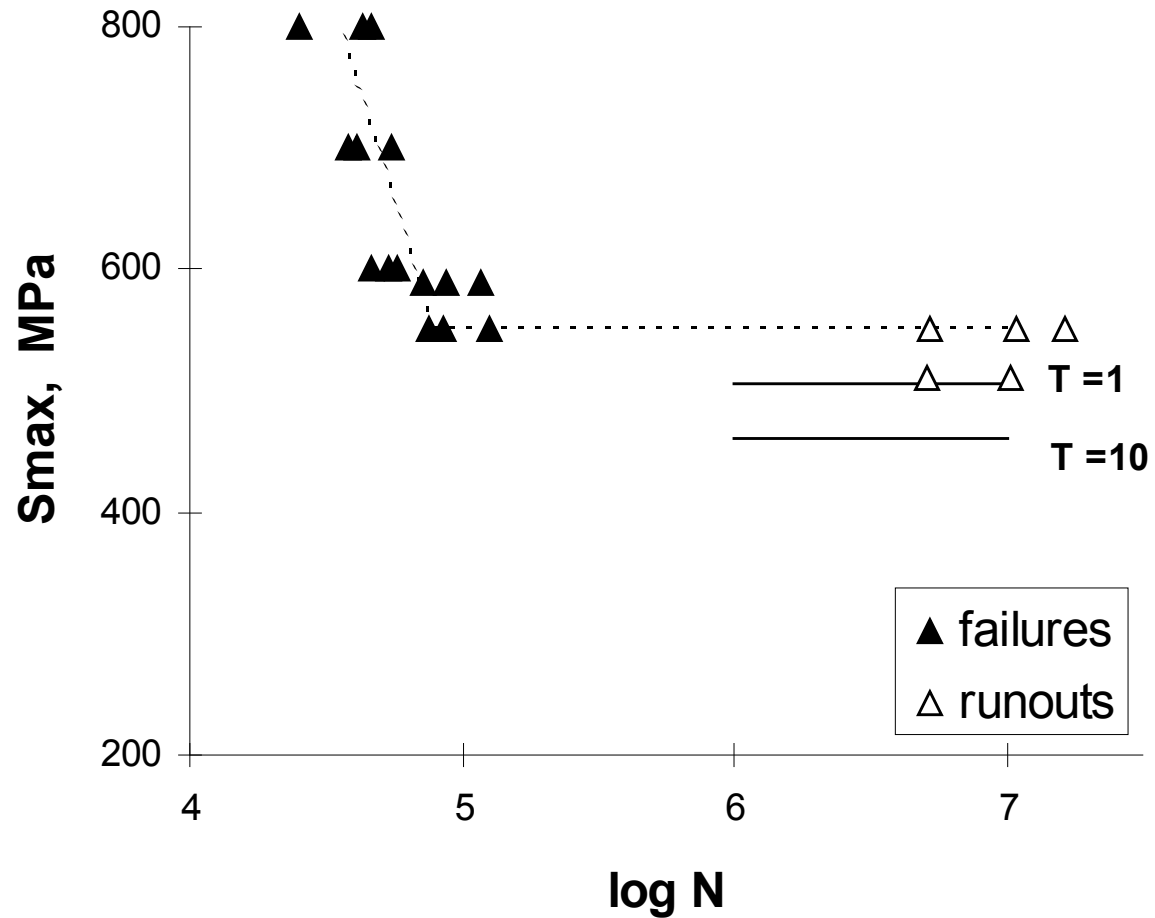
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SANDVIK Materials Technology

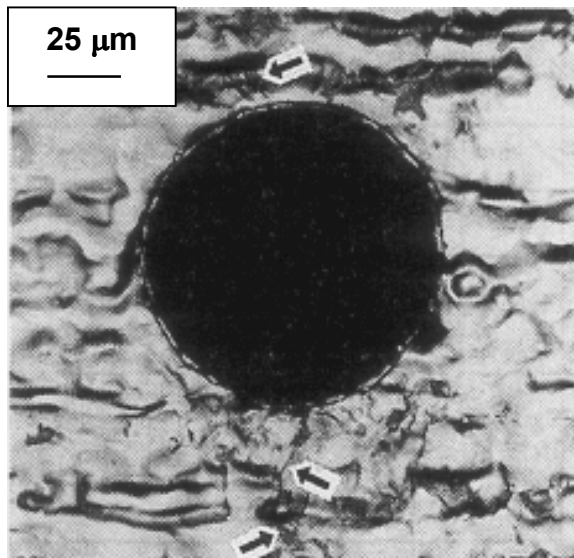
What is the fatigue limit ?



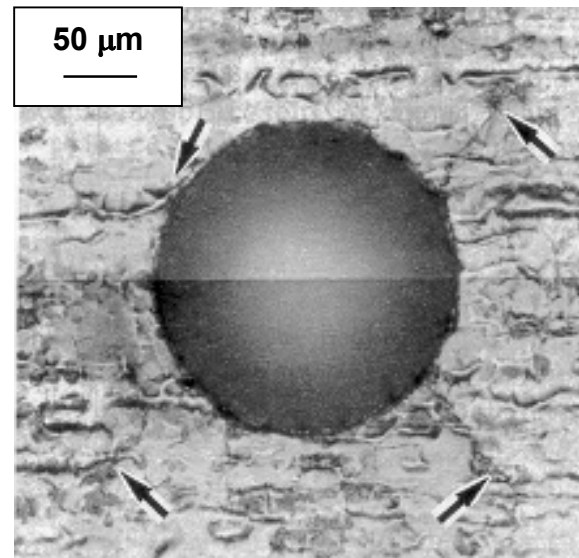
Defects and fatigue strength

Murakami's experiments on specimens containing microholes

Axial loading (bending)



torsional loading (biaxial)

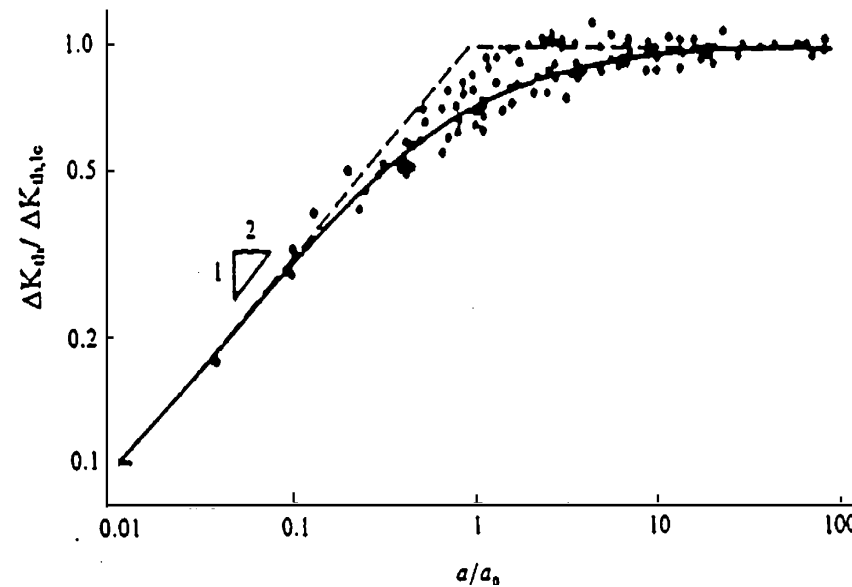
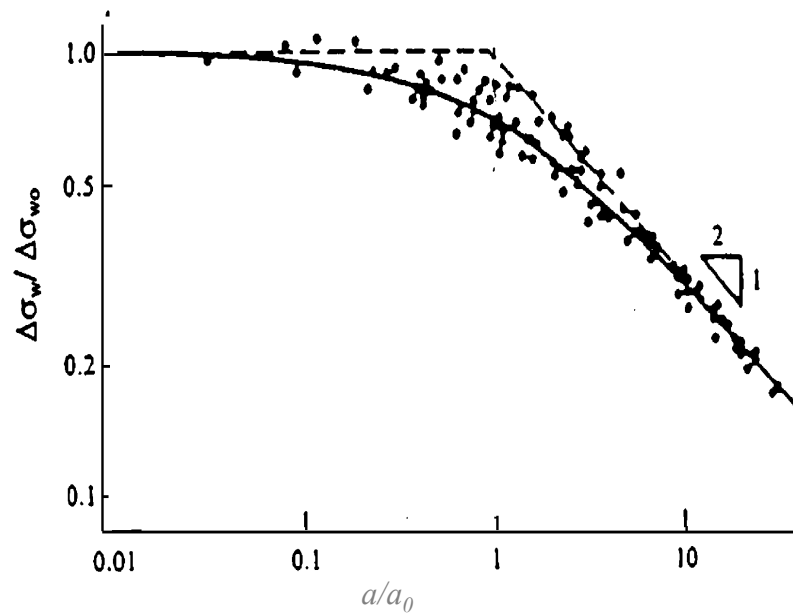


Fatigue limit is the **'non-propagation' condition** for small cracks emanating from the defects

Short cracks and defects

Murakami's idea:

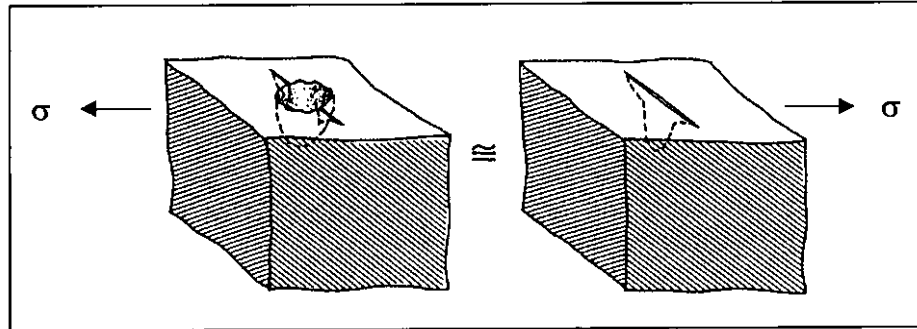
- defects can be treated as short cracks;



threshold ΔK e Δs_{lim} depend on the crack dimension



$\sqrt{\text{area}}$ model (Murakami & Endo)



Murakami's
equation:

$$\Delta K_I = 0.65 \cdot \Delta \sigma \cdot \left(\pi \cdot \sqrt{\text{Area}} \right)^{1/2}$$

Thresholds:

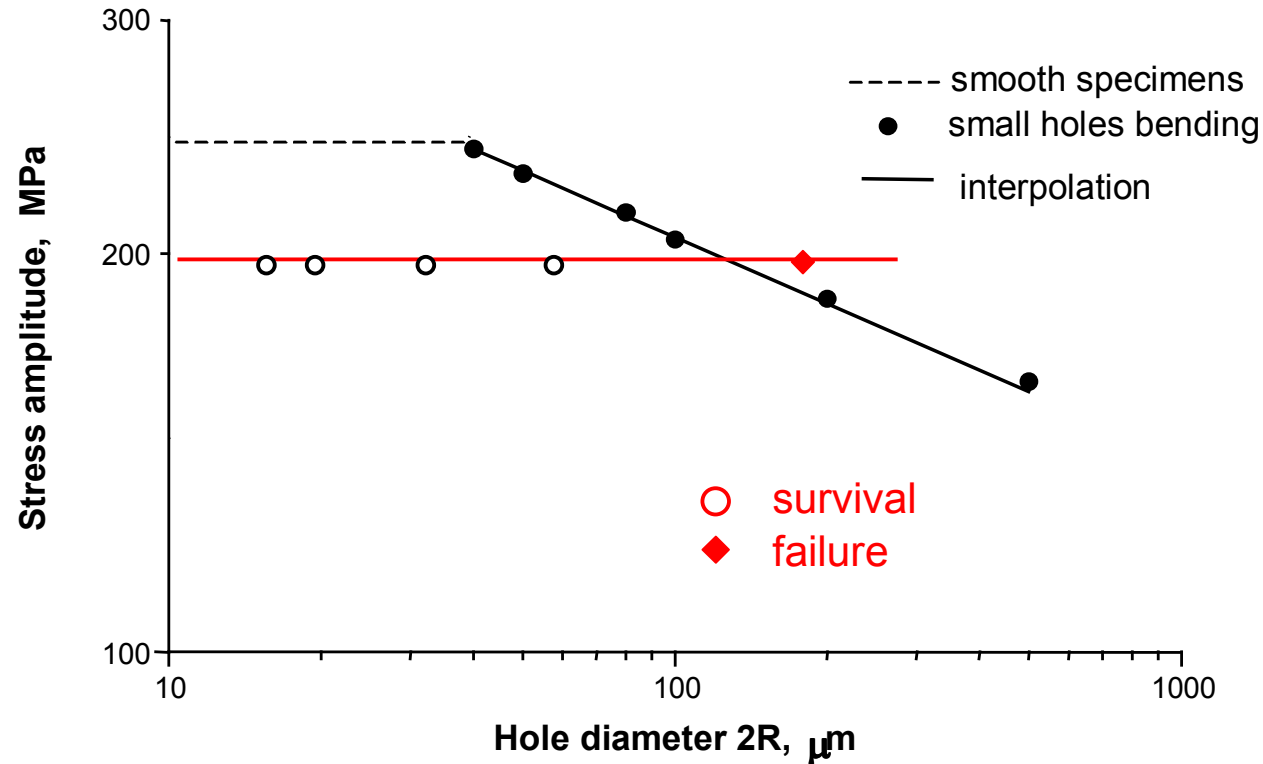
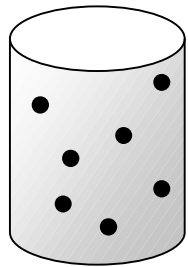
$$\Delta K_{th} = 3.3 \cdot 10^{-3} \cdot (Hv + 120) \cdot \left(\sqrt{\text{area}} \right)^{1/3} \cdot (0.5 - R/2)^{0.226 + Hv \cdot 10^{-4}}$$

Fatigue limit:

$$\sigma_w = C \cdot \frac{(Hv + 120)}{\sqrt{\text{area}}^{1/6}} \cdot (0.5 - R/2)^{0.226 + Hv \cdot 10^{-4}}$$

C = 1.56 internal def.
C = 1.43 surface def.

Extreme defects

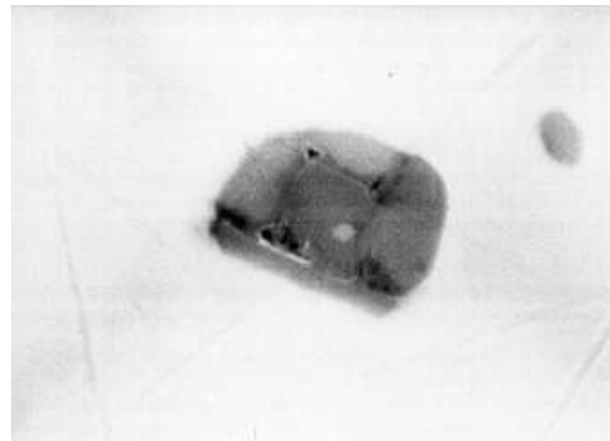
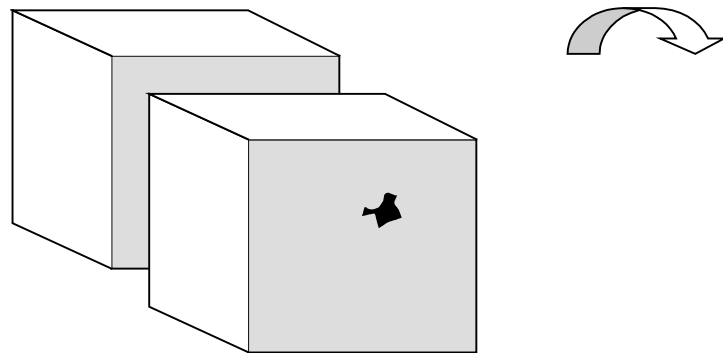
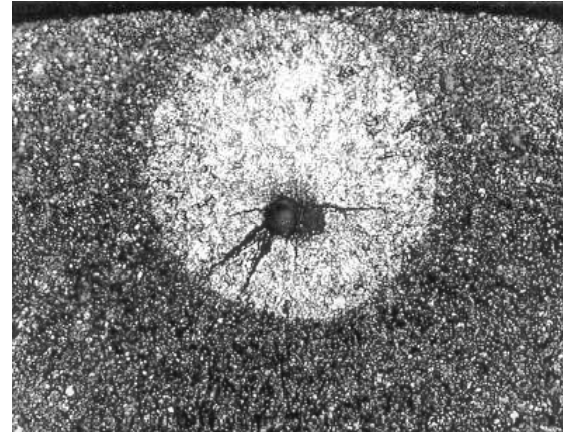
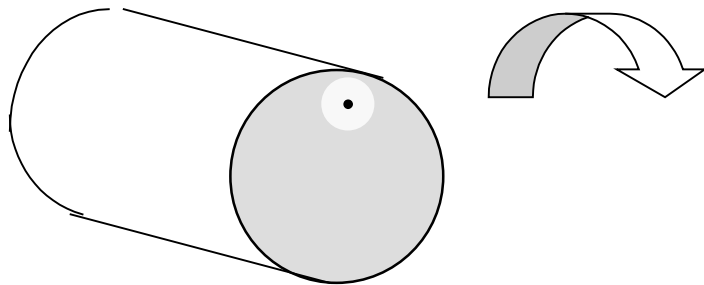


the fatigue is controlled by the **extreme values** of the population of defects **not** by the average dimension



analysis of extremes based on **extreme value sampling**

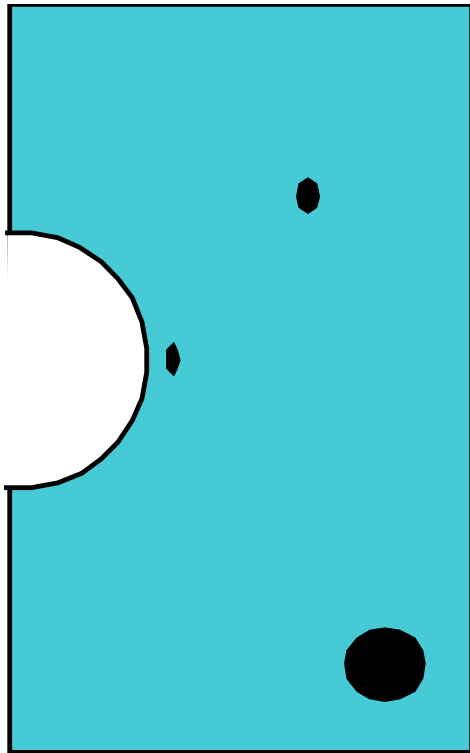
Extreme defects



- Methods based on Statistics of Extremes
- new technical recommendations (ESIS e ASTM)

Components with defects

?



Weakest-link model



Application to 3 strips of
'super-clean' steels



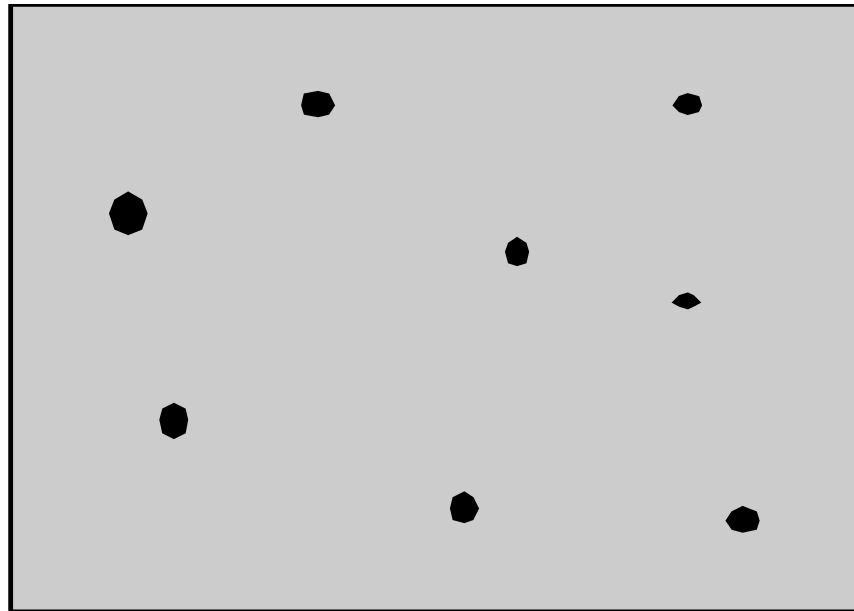
Comparison with fatigue
experiments

Extremes

Let us consider **m defects** with distribution function F

the distribution
function of the
maximum defect:

$$F_{\max}(a) = [F(a)]^m$$

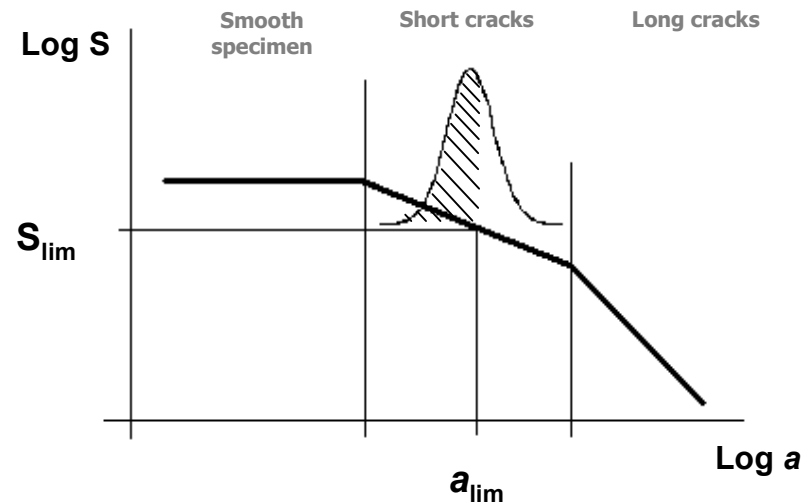
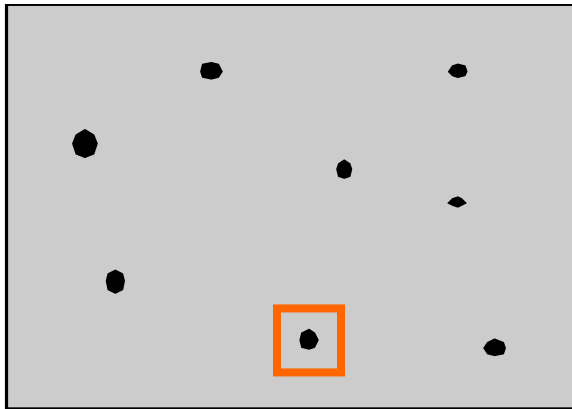


$$m \rightarrow \infty$$

$$F_{\max}(a) \cong G(a, \lambda, \delta) = \exp \left(-\exp \left(-\frac{a - \lambda}{\delta} \right) \right)$$

Extremes \Rightarrow Weakest-link

m defects



Weakest-link

$$R_{tot} = R^m$$

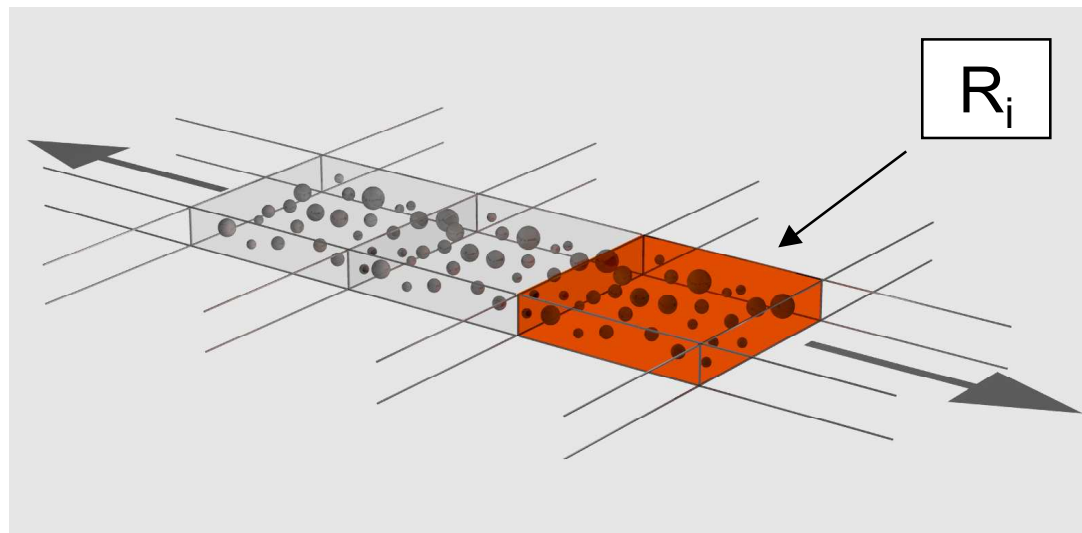
$$R = \{ \Pr (a \leq a_{lim}) \} = F (a_{lim})$$

$$R_{tot} = [F (a_{lim})]^m = \{ \Pr (a_{max} \leq a_{lim}) \}$$

Approaches of WL and Extremes are coincident

Weakest-link model

If we imagine the component divided into **n domains**:



Weakest-link

$$R_{tot} = \prod R_i \quad \rightarrow \quad R_i = G_V (a_{lim,i})$$

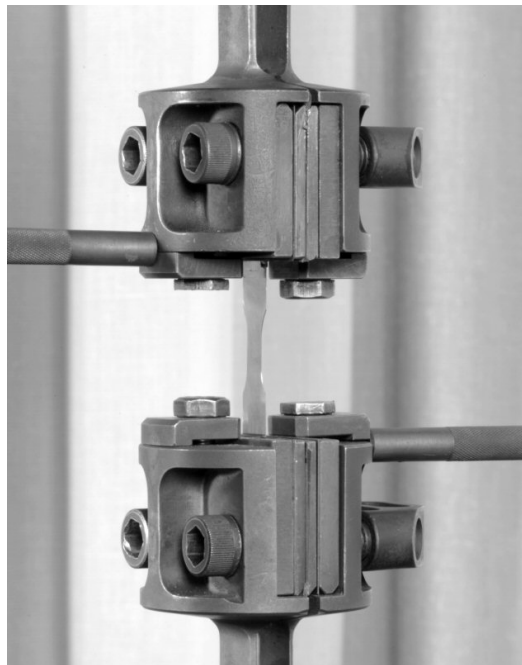
Extremes

$$G_V = (G_{V_0})^{\frac{V}{V_0}}$$

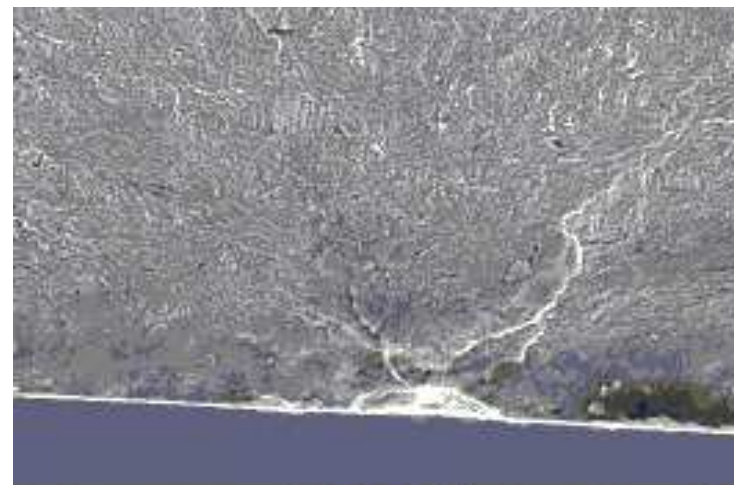
Application

3 series of thin strips of super-clean steels (SANDVIK)

Material	Thickness [mm]	HV [kgf / mm^2]	Rm [MPa]
strip A	0.305	539	1705
strip B	0.305	556	1744
strip C	0.381	581	1649

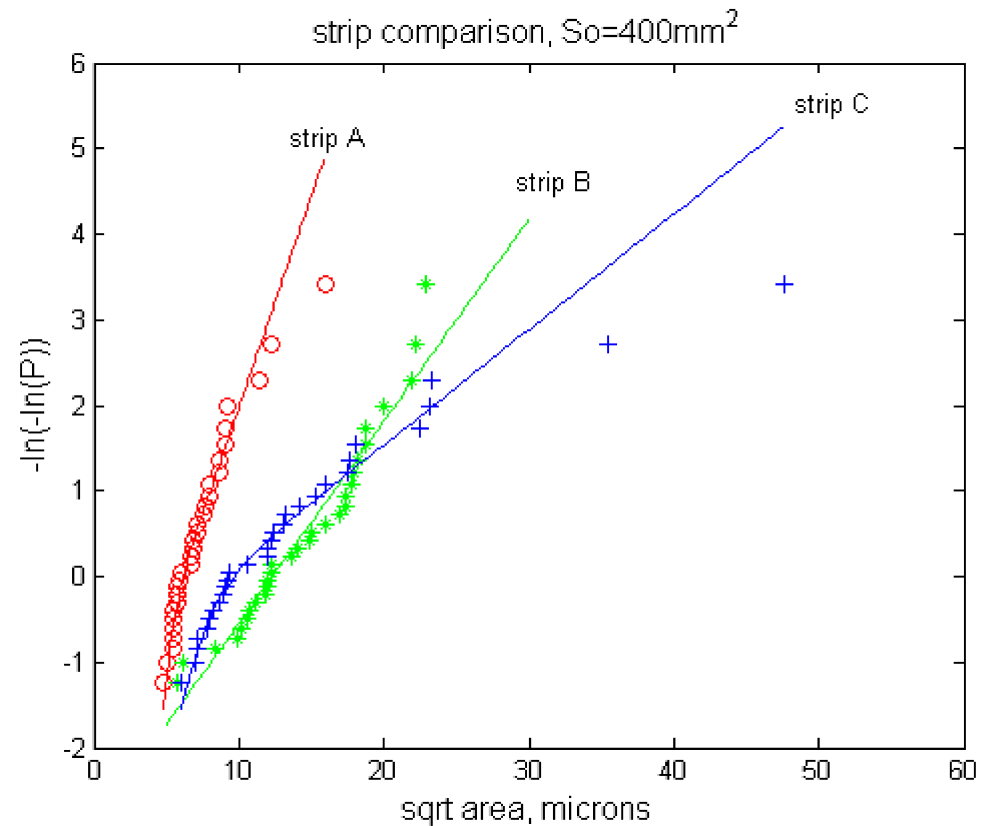


inclusions at fracture origin



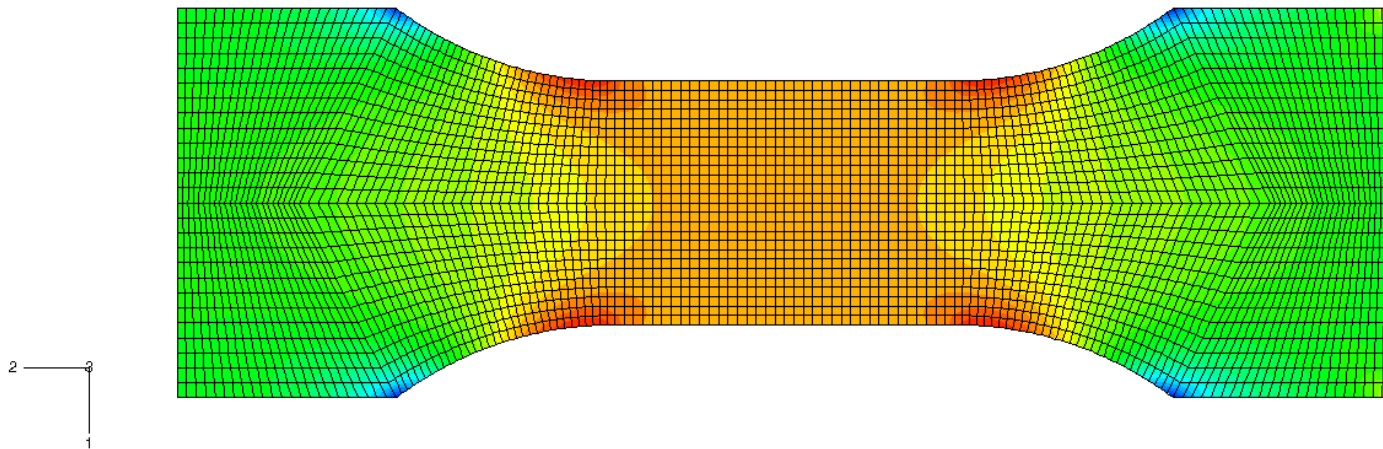
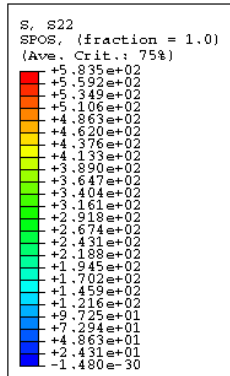
Research of extreme defects

Polished sections



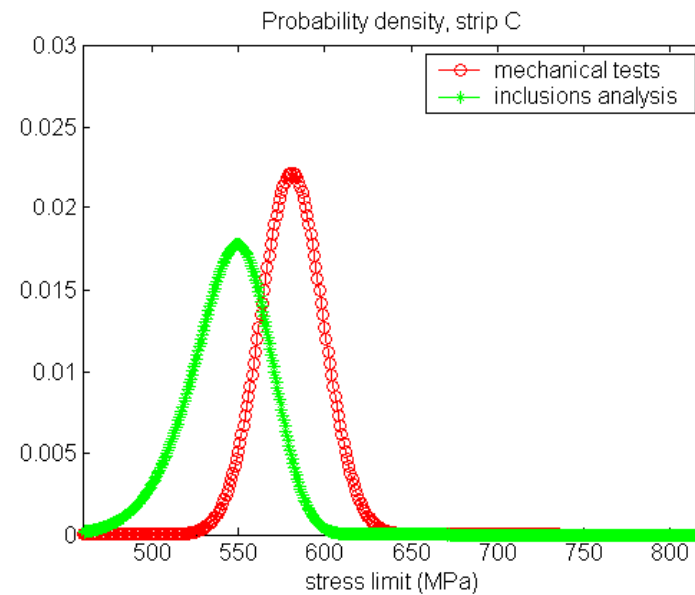
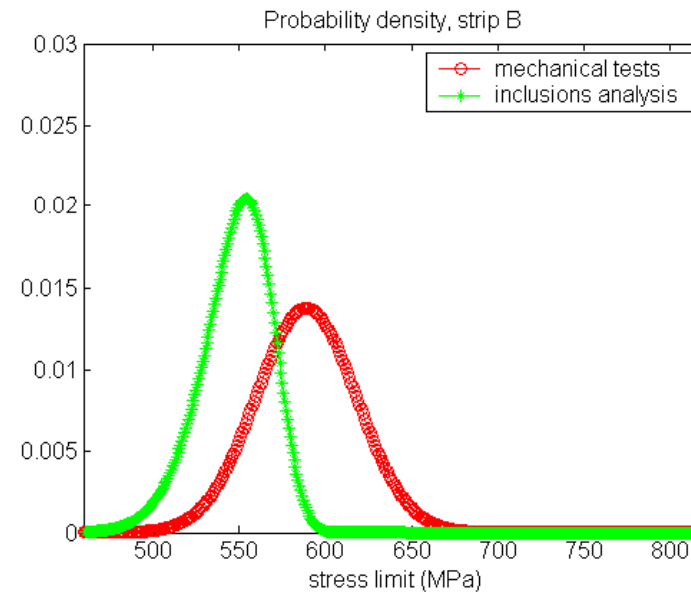
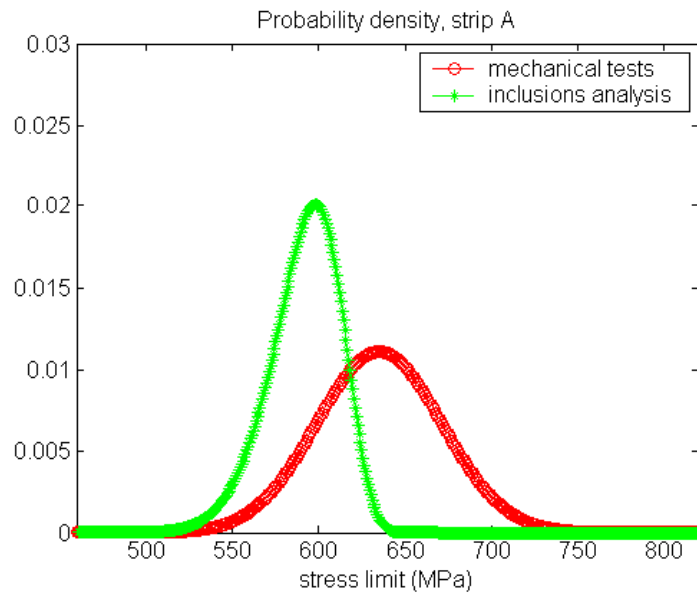
Distribution of maximum defects on $S_0 = 400 \text{ mm}^2$

FE analysis of fatigue specimens



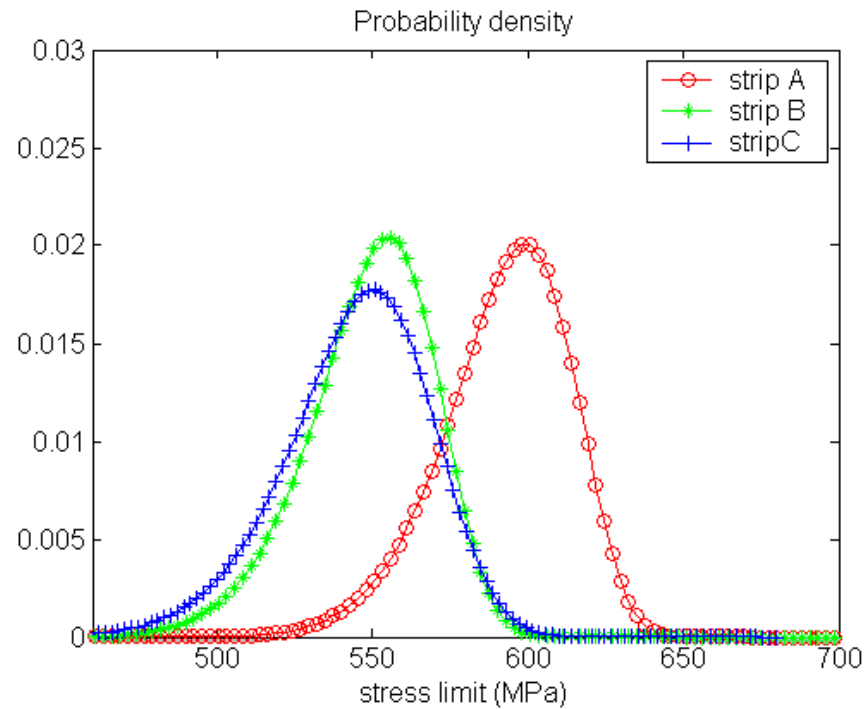
- Calculation of failure probability as a function of S ;
- determination of fatigue limit distribution function.

Results



good fatigue strength
predictions

Comparison among strips



strip B has the
best hardness

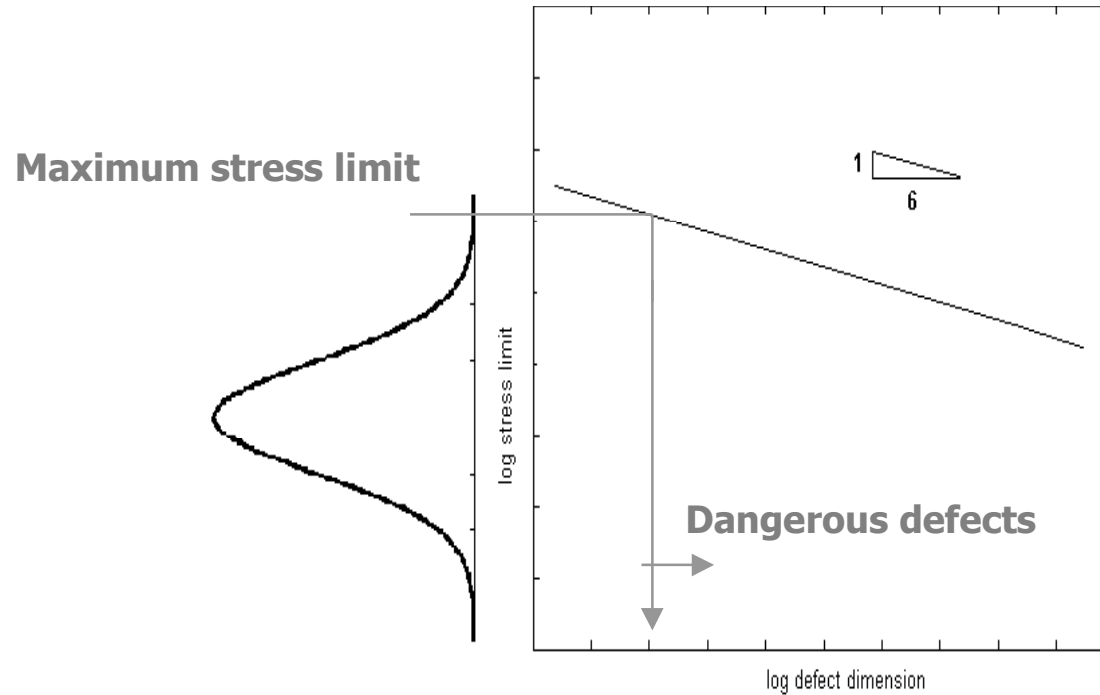


why low fatigue strength ?

extreme defects ?



Comparison among strips



Strip A	Strip B	Strip C	
7	11	11	Critical threshold [μm]
0.606	1.361	0.722	Critical density / $400 mm^2$

'density' of detrimental defects

Conclusions

- fatigue limit in presence of defects can be estimated from the Kitagawa diagram of the material under examination
- a Weakest-link model has been proposed in combination with 'statistics of extremes' for estimating fatigue strength in mechanical components
- application shows that while for material qualification the maximum defect is a sufficient information, the calculation of the failure probability for a component need also information about defect density