

The Finite Element Method for the Wave Equation

The Wave Equation

We consider the scalar wave equation modelling acoustic wave propagation in a bounded domain Ω^3 , with boundary Γ :

$$\begin{aligned} \frac{1}{c(\mathbf{x})^2} \frac{\partial^2 u}{\partial t^2} - \Delta u &= 0, \quad \text{in } \Omega \times (0, T), \\ u(\cdot, 0) &= 0, \quad \frac{\partial u}{\partial t}(\cdot, 0) = f, \quad \text{in } \Omega, \\ \partial_n u|_{\Gamma_1} &= 0, \quad \text{on } \Gamma \times (0, T), \end{aligned} \tag{1}$$

where $u(\mathbf{x}, t)$ is the pressure and $c(\mathbf{x})$ is the wave speed depending on $\mathbf{x} = (x_1, x_2, x_3) \in \Omega$, t is the time variable, T is a final time, and f is a load vector.

Finite Element Discretization

We now formulate a finite element method for (1) based on using continuous piecewise linear functions in space and time. We discretise $\Omega \times (0, T)$ in the usual way denoting by $K_h = \{K\}$ a partition of the domain Ω into tetrahedra K ($h = h(\mathbf{x})$ being a mesh function representing the local diameter of the elements), and we let $J_k = \{J\}$ be a partition of the time interval $(0, T)$ into time intervals $J = (t_{k-1}, t_k]$ of uniform length $\tau = t_k - t_{k-1}, k = 1, \dots, N$.

To formulate the finite element method for (1) we introduce the finite element space W_h^u defined by:

$$\begin{aligned} W^u &:= \{u \in H^1(\Omega \times J) : u(\cdot, 0) = 0, \partial_n u|_\Gamma = 0\}, \\ W_h^u &:= \{u \in W^u : u|_{K \times J} \in P_1(K) \times P_1(J), \forall K \in K_h, \forall J \in J_k\}, \end{aligned} \tag{2}$$

where $P_1(K)$ and $P_1(J)$ are the set of piecewise linear functions on K and J , respectively.

Fully discrete scheme

To obtain discrete scheme we apply CG(1) in space and time and seek a discrete solution in the space W_h^u for u spanned by the functions

$$u(x, t) = \sum_{l=0}^N \sum_{i=1}^M u_i^l \varphi_i(x) \psi_l(t),$$

where $\varphi_i(x)$ and $\psi_l(t)$ are standard continuous piecewise linear functions in space and time, respectively.

Substituting this into (1), we obtain the following system of linear equations:

$$M(\mathbf{u}^{k+1} - 2\mathbf{u}^k + \mathbf{u}^{k-1}) = \tau^2 F^k - \tau^2 A\left(\frac{1}{6}\mathbf{u}^{k-1} + \frac{2}{3}\mathbf{u}^k + \frac{1}{6}\mathbf{u}^{k+1}\right), \quad k = 1, \dots, N-1, \quad (3)$$

with initial conditions :

$$u(0) = \left. \frac{\partial u}{\partial t} \right|_{t=0} = 0. \quad (4)$$

Here, M is the mass matrix in space, A is the stiffness matrix, F^k is the load vector at time level t_k , $k = 1, 2, 3 \dots$, \mathbf{u} is the unknown discrete field values of u , and τ is the time step.

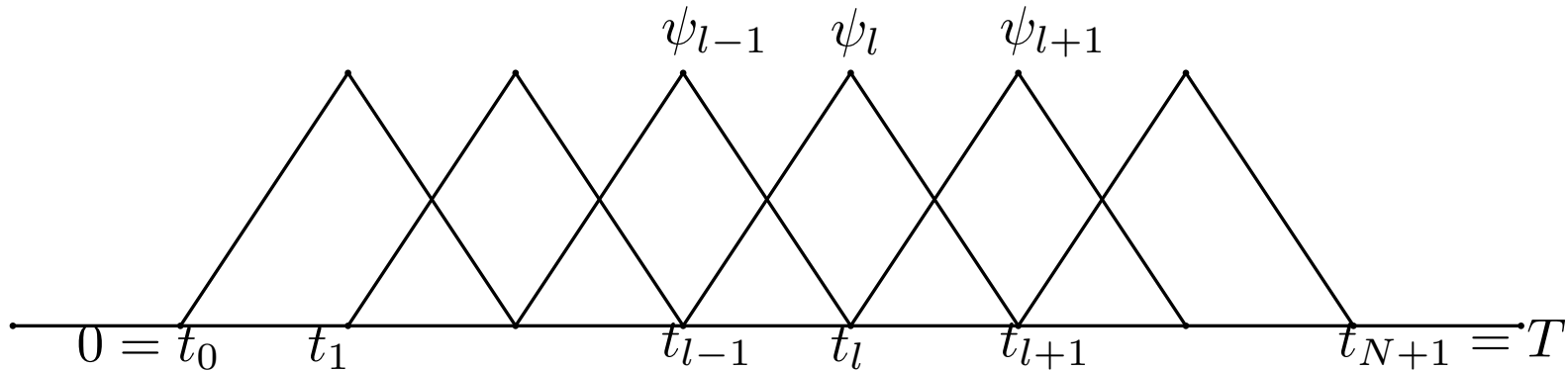
The explicit formulas for the entries in system (3) at each element e can be given as:

$$\begin{aligned}M_{i,j}^e &= \left(\frac{1}{c^2}\varphi_i, \varphi_j\right)_e, \\K_{i,j}^e &= (\nabla\varphi_i, \nabla\varphi_j)_e, \\F_j^e &= (f, \varphi_j)_e,\end{aligned}\tag{5}$$

where $(\cdot, \cdot)_e$ denotes the $L_2(e)$ scalar product. The matrix M_e is the contribution from element e to the global assembled matrix in space M , K^e is the contribution from element e to the global assembled matrix K .

W_h^u is a finite dimensional vector space, $\dim W_h^u = M \times N$, with a basis consisting of the standard continuous piecewise linear functions $\{\varphi_i\}_{i=1}^M$ in space and hat functions $\{\psi_l\}_{l=1}^N$ in time, where:

$$\psi_l(t) = \begin{cases} 0, & \text{if } t \notin [t_{l-1}, t_{l+1}], \\ \frac{t-t_{l-1}}{t_l-t_{l-1}}, & \text{if } t \in [t_{l-1}, t_l], \\ \frac{t_{l+1}-t}{t_{l+1}-t_l}, & \text{if } t \in [t_l, t_{l+1}]; \end{cases} \quad (6)$$



The discrete system of equations

Using basis of functions $\{\varphi_i\}_{i=1}^M$ in space and $\{\psi_l\}_{l=1}^N$ in time we have:

$u_h = \sum_{l=0}^N \sum_{i=1}^M u_{hi}^l \varphi_i(x) \psi_l(t)$. Substituting into (1) we get:

$$\begin{aligned}
 & - \sum_{l=0}^N \sum_{i=1}^M u_{hi}^l \int_{\Omega} \frac{1}{c^2} \varphi_i(x) \int_{t_{l-1}}^{t_{l+1}} \frac{\partial \psi_l(t)}{\partial t} \frac{\partial v(x, t)}{\partial t} dx dt \\
 & + \sum_{l=0}^N \sum_{i=1}^M u_{hi}^l \int_{\Omega} \int_{t_{l-1}}^{t_{l+1}} \nabla \varphi_i(x) \nabla v(x, t) \psi_l(t) dx dt \quad (7) \\
 & = \int_{\Omega} \int_0^T f(x) v(x, t) dx dt \quad \forall v \in W_h^u.
 \end{aligned}$$

We take $v(x, t) = \varphi_j(x)\psi_m(t)$ and get:

$$\begin{aligned}
& - \sum_{l=0}^N \sum_{i=1}^M u_{hi}^l \int_{\Omega} \frac{1}{c^2} \varphi_i(x) \varphi_j(x) \int_{t_{l-1}}^{t_{l+1}} \frac{\partial \psi_l(t)}{\partial t} \frac{\partial \psi_m(t)}{\partial t} dx dt \\
& + \sum_{l=0}^N \sum_{i=1}^M u_{hi}^l \int_{\Omega} \nabla \varphi_i(x) \nabla \varphi_j(x) \int_{t_{l-1}}^{t_{l+1}} \psi_l(t) \psi_m(t) dx dt \quad (8) \\
& = \int_{\Omega} \int_0^T f(x) v(x, t) dx dt \quad \forall v \in W_h^u.
\end{aligned}$$

Let $U = u_{h_i}^l$ denote the vector of unknown coefficients,
 $M = (m_{ij})$, $A = (a_{ij})$ are mass and stiffness matrices $M \times M$ in space,
correspondingly, with coefficients

$$\begin{aligned} m_{ij} &= \int_{\Omega} \varphi_i(x) \varphi_j(x) dx, \\ a_{ij} &= \int_{\Omega} \nabla \varphi_i(x) \nabla \varphi_j(x) dx, \end{aligned} \tag{9}$$

$P = (p_{lm})$, $K = (k_{lm})$ are stiffness and mass matrices $N \times N$ in time
with coefficients

$$\begin{aligned} k_{lm} &= \int_{t_{l-1}}^{t_{l+1}} \frac{\partial \psi_l(t)}{\partial t} \frac{\partial \psi_m(t)}{\partial t} dt, \\ k_{lm} &= \int_{t_{l-1}}^{t_{l+1}} \psi_l(t) \psi_m(t) dt, \end{aligned} \tag{10}$$

and the load vector $b = (b_{jm})$ with coefficients

$$b_{jm} = \int_{\Omega} \int_{t_{l-1}}^{t_{l+1}} f(x) \varphi_j(x) \psi_m(t) dx dt. \quad (11)$$

First, we compute $K = (k_{lm})$ and $P = (p_{lm})$. Note, that $k_{lm} = 0, p_{lm} = 0$ unless $l = m - 1, l = m, l = m + 1$. Using the definition of test functions (6), we compute first diagonal elements k_{ll} :

$$\begin{aligned}
k_{ll} &= \int_{t_{l-1}}^{t_{l+1}} \psi'_l(t) \psi'_l(t) dt \\
&= \int_{t_{l-1}}^{t_l} \left(\frac{1}{\tau}\right)^2 dt + \int_{t_l}^{t_{l+1}} \left(\frac{-1}{\tau}\right)^2 dt = \frac{2}{\tau}, \\
p_{ll} &= \int_{t_{l-1}}^{t_{l+1}} \psi_l(t) \psi_l(t) dt \\
&= \int_{t_{l-1}}^{t_l} \left(\frac{t - t_{l-1}}{\tau}\right)^2 dt + \int_{t_l}^{t_{l+1}} \left(\frac{t_{l+1} - t}{\tau}\right)^2 dt = \frac{2}{3}\tau,
\end{aligned} \tag{12}$$

Similarly,

$$\begin{aligned}
k_{l,l+1} &= \int_{t_{l-1}}^{t_{l+1}} \psi'_l(t) \psi'_{l+1}(t) dt \\
&= \int_{t_l}^{t_{l+1}} \frac{-1}{\tau} \frac{1}{\tau} dt \\
&= -\frac{1}{\tau}, \\
k_{l-1,l} &= \int_{t_{l-1}}^{t_{l+1}} \psi'_{l-1}(t) \psi'_l(t) dt \\
&= \int_{t_{l-1}}^{t_l} \frac{-1}{\tau} \frac{1}{\tau} dt \\
&= -\frac{1}{\tau}.
\end{aligned} \tag{13}$$

Verification: write (6) for ψ_{l+1} and ψ_{l-1} and insert then into (14).

$$\begin{aligned}
p_{l,l+1} &= \int_{t_{l-1}}^{t_{l+1}} \psi_l(t) \psi_{l+1}(t) dt \\
&= \int_{t_{l-1}}^{t_l} \left(\frac{t - t_{l-1}}{\tau} \right) \cdot \left(\frac{t - t_l}{\tau} \right) dt \\
&= \frac{1}{6} \tau, \\
p_{l-1,l} &= \int_{t_{l-1}}^{t_{l+1}} \psi_{l-1}(t) \psi_l(t) dt \\
&= \int_{t_l}^{t_{l+1}} \left(\frac{t_{l+1} - t}{\tau} \right) \cdot \left(\frac{t_l - t}{\tau} \right) dt \\
&= \frac{1}{6} \tau.
\end{aligned} \tag{14}$$

Verification: write (6) for ψ_{l+1} and ψ_{l-1} and insert then into (14).

We compute coefficients of b in the same way to get:

$$\begin{aligned}
b_{jm} &= \int_{\Omega} \int_{t_{m-1}}^{t_{m+1}} f(x) \varphi_j(x) \psi_m(t) \, dx dt \\
&= \int_{\Omega} f(x) \varphi_j(x) \int_{t_{m-1}}^{t_m} \frac{t - t_{m-1}}{\tau} \, dx dt \\
&\quad + \int_{\Omega} f(x) \varphi_j(x) \int_{t_m}^{t_{m+1}} \frac{t_{m+1} - t}{\tau} \, dx dt \\
&\approx \tau \int_{\Omega} f(x_j) \varphi_j(x) \, dx.
\end{aligned} \tag{15}$$

We substitute computed coefficients to (8) and get the system of linear equations (3):

$$M(\mathbf{u}^{k+1} - 2\mathbf{u}^k + \mathbf{u}^{k-1}) = \tau^2 F^k - \tau^2 A\left(\frac{1}{6}\mathbf{u}^{k-1} + \frac{2}{3}\mathbf{u}^k + \frac{1}{6}\mathbf{u}^{k+1}\right), \quad k = 1, \dots, N - 1. \quad (16)$$

To obtain an explicit scheme we approximate M with the lumped mass matrix M^L in space, the diagonal approximation obtained by taking the row sum of M , as well use mass lumping in time by replacing the terms $\frac{1}{6}\mathbf{u}^{k-1} + \frac{2}{3}\mathbf{u}^k + \frac{1}{6}\mathbf{u}^{k+1}$ by \mathbf{u}^k . By multiplying (16) with $(M^L)^{-1}$ we obtain an efficient explicit formulation:

$$\mathbf{u}^{k+1} = \tau^2 F^k + 2\mathbf{u}^k - \tau^2 (M^L)^{-1} K \mathbf{u}^k - \mathbf{u}^{k-1}, \quad k = 1, \dots, N - 1, \quad (17)$$